Lake Matthew Team / Celestia

SEC presentation, Lake Matthew Team & Martin Lade

Aug 27 2017

Rationale for the Omaha Trail MATT: The Mars Terraformer Transfer Omaha Crater: Cargo & Propellant Deimos ISRU, Deimos Dock Deimos Rail Launcher (DRL) Mars Lift (ML) Tramway Omaha Trail Benefits

MATT + Omaha Trail

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Rationale for the Omaha Trail

MATT: The Mars Terraformer Transfe Omaha Crater: Cargo & Propellan Deimos ISRU, Deimos Dock Deimos Rail Launcher (DRL) Mars Lift-(ML)

Iramway Omaha Trail Benefits MATT + Omaha Trail

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Objective for the Omaha Trail:

• High-efficiency transport infrastructure to Lake Matthew facilities at Omaha Crater

Rationale for the Omaha Trail:

- It would reduce the number of required Earth launches
- It would lower cargo transport cost
- An integrated system orchestrates and justifies R&D for each infrastructure component
- It would enable faster crew return with less cosmic radiation exposure

MATT: The Mars Terraformer Transfer MATT - Omaha Trail

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Terraformation

Benefits of Terraformation

- Cuts mass, energy and labor needed
- Cuts R&D cost
- Enables scaled ISRU for self-sufficiency
- Follow-on benefit: Sole-source contracts for Mars facilities, provisions and rare metals

Practical Terraformation

- Impactor example:
 - Bedrock to +50 °C
 - Meltwater
 - Air pressure > 1 kPa
 - Lake formation possible
- This is the common, natural way to terraform a site on Mars



Practical Terraformation



MATT

• Mars Terraformer Transfer



LakeMatthew.com

DE-STARLITE System

- "DE-STAR": "Directed Energy System for Targeting of Asteroids and exploRation"
- "LITE":

a small version for singlelaunch configuration ("Shepherd")

Lubin et al. 2016

Flight Plan (NDA)

- Shepherd: COTS, single-launch payload
- Tracking and trajectory changes: <100 m at Mars
- The impact occurs in 2036
- Impact: 9 km crater, structured depressions, 9 km² heat lens, > 1 kPa, new lowest point on Mars
- Result: Lake Matthew



Omaha Crater – Designated Impact Site

- Ice abundant locally in near-surface
- Freshwater stable to 11 °C, for persistent Lake Matthew and other reservoirs



Omaha Crater



ALAN SIGA 1 Jonathan S Blair/National Geographic/Getty Images n, Lake Matthew & Martin Lades Tool

Habitat and Greenhouse Domes



Mining

• Principal rare metals in Type IVA meteorite, at scale of 16 Psyche:

Element	Concentration (ppm) by mass	Value at current pricing (\$)
Platinum	6.2	\$ 2,093,000,000,000,000,000
Palladium	4.0	\$ 1,268,000,000,000,000,000
Rhodium	2.8	\$ 1,038,000,000,000,000,000
Gold	1.6	\$ 698,000,000,000,000,000



Davis 2005, D'Orazio & Folco 2003, Hoashi et al. 1993, Shen et al., 1996

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Mining

Article in press: "A Station at the End of Musk's Railroad"



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Palladium	4.0	\$ 1,268,000,000,000,000,000
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Gold	1.6	\$ 698,000,000,000,000,000

MATT In Context

From Omaha Crater to the Omaha Trail:

- At Omaha Crater, Mars' paucity of natural resources and severity of environment no longer constrain settlement growth, from 2036
- Transport efficiency becomes the constraint
- Hence the Omaha Trail



Rationale for the Omaha Trail MATT: The Mars Terraformer Transfer Omaha Crater: Cargo & Propellant omos ISRU, Deimos Dock mos Rail Launcher (DRL) Mars Lift (ML) Tamway

Omaha Trail Benefits VIATT + Omaha Trail

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Omaha Crater ISRU

- Self-sufficiency in:
 - Breathing and propellant gases
 - Treated water and brine
 - Bulk fertilizer, hydroponic sand
 - Staple foods
 - Most construction materials
- Hence ~90% cut in cargo

Omaha Crater Cargo

- Cargo required for:
 - Construction titanium powder, ETFE foil
 - Complex tools and parts
 - Industrial gases, reactants, catalysts
 - Medical supplies
 - Novelty foods
- Most mass of cargo ships devoted to:
 - Propellant
 - 1950 tons propellant
 - 450 tons cargo
 - 150 tons dry mass



Omaha Crater Propellant

- Total propellant per cargo flight: 87,000 tons
- Cargo with Mars surface propellant: 300 tons
- Cargo with LMO propellant: 450 tons
- Incentive to tank up in Mars orbit
- Incentive to perform ISRU in Mars orbit



SpaceX

Deimos ISRU, Deimos Dock limos Rail Launcher (DRL)

- Deimos density: 1.5 g/cm³ (Murchie et al. 2013)
- ~50 wt% volatiles, within 20-60 m of polar surface (Fanale and Salvail 1990)
- Products: oxygen, methane, treated water
- Methods: CAVoR, alternate coal gasification reactions (Nichols 1993)







- (a) hypothetical South Pole volatile mining site, 1 km diameter crater / depression
- (b) and (c) summer-shaded craters, best for cryogenic storage
- (d) sunlit crater, best for water storage



Chuck Clark



Deimos Dock

North



Lake Matthew Team / Tayfun Öner / USGS / Peter Thomas

L1

to CW



Deimos Dock

- Value:
 - Propellant is produced at 4x Mars surface rate, due to 4x cumulative PV
 - Maximized delta-v, with Deimos-Mars round-trip fueling at Deimos Dock
 - 100% of Omaha Crater power is freed for use on Mars
 - Deimos hot mining waste is efficiently converted to shields and counterweights
 - Deimos is a proving ground for tech used elsewhere on the Omaha Trail
 - Deimos provides a vacuum platform, recoil mass, and ISRU products useful for a Deimos Rail Launcher (DRL)

Omaha Trail

Rationale for the Omaha Trail MATT: The Mars Terraformer Transfer Maha Crater: Cargo & Propellant SRU, Deimos Dock Deimos Rail Launcher (DRL)

Iramway Omaha Trail Benefits Crew Benefits

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Deimos Rail Launcher (DRL)

 Assisted launch of spacecraft from Deimos, in the spirit of a catapult launcher on an aircraft carrier



J.S. Navy

Deimos Rail Launcher (DRL)

- Value:
 - 1 km/s propellant-free delta-v
 - DRL is the most efficient conversion of Deimos PV into delta-v
 - Launch to Mars EDL or to Earth return insertion, with decision point at Mars periapsis (



Deimos Rail Launcher (DRL)

- Helical coil electromagnetic launcher: DRL considerations:
 - Highest efficiency of a rail launcher: >80% with LOX superconducting coils
 - Runs off HVDC power at high voltage for low losses
 - Bidirectional armature for acceleration and deceleration
 - Potentially adaptable to lightweight tether frame tensioned with counterweight and power line repulsion




- Possibility of platform without wheels, mounted e.g. with repulsive Lorentz tubes
- Superconducting operation: armature with LOX dewar, and stator with LOX fill
- Gentle acceleration: e.g., 0.5 m/s² over 1000 km rollout
- Conservation of angular momentum clears Deimos



- Power:
 - 300 MW HVDC supplies ~600 gigajoules of energy during launch.
 - With 80% DRL efficiency, need an extra 2.8 terajoules
 - Superconducting magnetic energy storage (SMES) can supply
 - SMES can be low-mass on Deimos: vacuum operation at cryogenic LOX plant





Lake Matthew Team / Tayfun Öner / USGS / Peter Thomas



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Omaha Trail to Lake Matthew

Rationale for the Omaha Trail MATT: The Mars Terraformer Transfer Omaha Crater: Cargo & Propellant Deimos ISRU, Deimos Dock Camos Rail Launcher (DRL) Mars Lift (ML)

Iramway Omaha Trail Benefits MATT + Omaha Trail



Mars Lift for Omaha Trail to Lake Matthew

M. Lades, part of combined presentation with MATT/Lake Matthew Team

Mars Lift



• Value:

- Space Elevators follow the Railway Paradigm:
 - Invest in infrastructure, reap benefits from it.
- Case for a Mars Space Elevator
 - Save a drastic percentage of propellant compared to landing rockets on the planet and taking off again for faster buildup of Mars infrastructure.
 - Lighter demands than Earth due to the Mars-Moons System promising a lighter feasibility condition.
- Mars Lift
 - Reduced requirements for an architecture as close as possible to implementation.
 - Branding distinction from Earth Space Elevator.



Boundary Conditions for Mars Lift

Plus

- 1. Lower gravity of Mars (~ 1/3 Earth) and similar rotation speed (ω) => better for elevators than Earth
- 2. Moons, with elevators

Minus

- 1. Moons, to avoid
- 2. Dust storms up to 80 km altitude ⇔ Not even the highest peaks avoid them, (Clancy, 2008)
- 3. Static electricity in the Martian atmosphere ⇔ ~2 orders of magnitude higher conductivity than Earth. More frequent discharges (lightning)
- 4. Remote environment 🗢 Everything has to be brought in at first. In situ resource utilization (ISRU) is imperative for the whole Mars Lift concept.

and the Elevator Feasibility Condition



Moons

Phobos







- Mars radius: 3396 km
- km from Mars center (above surface) 9380 (5840)
- Orbit period: 27600 s (Mars days) 0.319
- Projected speed over ground: 1920 km/h
- Mass: 1.072 10¹⁶ kg
- Radius: 11.1 km

23436 (~20100) 109000 s 1.262

162 km/h (retrograde) 1.5 10¹⁵ kg 6.2 km

 Areostationary Orbit, km from Mars center (above surface): 20427 (17031) ISEC

Options for Mars Lift



1. Use the Moons

- Phobos Tethers
 - Drop Tether of ~5740 km to avoid Mars atmosphere
 - Phobos Elevators L1, L2
- Deimos Tethers
 - Deimos Elevators, L1, L2



(Penzo, P., July 1984)

2. Avoid the Moons

- Off-Equator Mars Lift to avoid the moons
- 1. Use mountains (Olympus Mons, etc.) to avoid dust
- 2. Do not use mountains



Conclusions: Elevators for Mars Lift

Phobos Drop Tether

- + Avoids dust storms and electrostatic charge of the Mars atmosphere
- + Is the shortest possible tether of only ~6000 km
- 100 km vertical remain to be bridged
- Terminal velocity in Mars atmosphere is ~1000 km/h
- Even taking the lateral 1920 km/h of Phobos out with some other constructs, the vertical fall is hard to brake
- Braking a 100 km fall
 - Mars atmosphere: ~600 Pa, 0.6% of Earth. There will be no hypersonic aerodynamic Mars cargo planes!
 - Adding a parachute to every container or similar seems impractical
 - Rockets burn propellant, which we are trying to avoid. ~3 mt per 10 mt cargo container, prohibitive
 - Infrastructure to brake the containers from the ground would be huge and therefore appears also prohibitive
- \Rightarrow Mars atmosphere is just dense enough to be annoying but not useful
- \Rightarrow Drop tether economics appears undesirable

• Ground Tether, has to be

- robust against dust or requires a cleaning mechanism
- protected against electric discharge
- clear of the moons, therefore needs to be deployed off the equator
- almost ~20000 km long (or longer, clearing Deimos)

⇒ Conclusion: Ground Tether further Investigated



Mars Lift, Feasibility Condition



Version 2.0/Mars of the feasibility condition (work in progress):

- 1. The usual leaky integrator equation for the constructed/decaying tether that needs to be regularly serviced to remain in operation.
- 2. Moves from sums to factors where possible, stronger optimization criterion.
- 3. Includes a Geometry Condition: Irrespective of tether strength, a minimal tether size/surface area needs to be provided for climbers/rappellers to operate.
- 4. No Capstaning (wrapping around the wheels) for vehicles on Space Elevators
- For Mars Lift, the direction is down and no climber motors or (almost no) power sources are necessary. Service/material comes from Deimos.



Candidate Anchor Site 1, Elevator Peak

- Elevator Peak
 - ~ 6200 m Elevation
 - 18 S, 59.5 W





ISEC

Candidate Anchor Site 2, Pinnacle Station



- Morava Valles
 - ~ -2000 m
 - 12.65 S, 23.6 W

Pinnacle Station 212.65 S, 23.6 W

Morava Valles

Image NASA / USGS ESA / DLR / FU Berlin (G Neukum)

Google Earth

Imagery Date: 2/12/2009 12°50'55.70" S 23°45'27.64" W elev -2430 m eye alt 112.28 km 🔘



Mars Lift, Tether Strength and Taper



- Specific Strength in MYuri is the relevant variable for Space Elevators
 - MYuri is a derived unit equal to N/tex (with tex = g/km) and GPa/(g/cm³) or 10⁶ Nm/kg = 10⁶ m²/s²
 - We assume a specific mass of CNTs of $\rho=1.5$ g/cm³ (values 1.3 2 are common)
 - Investigated are typically two tether strengths $\sigma 0$ of:
 - 10 GPa => 6.6 MYuri
 - 20 GPa => 13.3 MYuri
 - Potential composed of gravitational pull, dependent on the distance from the center of gravity, and centrifugal force, dependent on distance from the rotation axis $V = -V0\left(\frac{r_s}{r} + \frac{1}{2}\frac{r_{\perp}^2}{r_s^2}\right)$ with $V0_{Mars} \approx 2.097 \text{ km}^2/\text{s}^2$
 - and the relationship between tether cross section on the ground and the maximum at the aerostatic orbit is: $\frac{T}{T0} = \frac{A}{A0} = e^{\frac{P}{C0}\Delta v}$
- Taper factors
 - 10 GPa tether: 4.15 (just tether, no loads) with A0 = 50 mm² (10x safety factor for 20 GPa) =>
 - 20 GPa tether: 2.03 (just tether, no loads) bracket for Tether Mass: ~1700 mt



The curvature follows the tether shape equation

Curvatures for 10 GPa and 20 GPa tethers anchored at18° latitude for Elevator Peak:



- Clearance of moving Phobos orbit requires at least 185 km from the equator at Phobos orbit (brown ellipse) (1.12° latitude, Jacobson/Lainey, 2014)
- Presented are first approximative results. Shape will slighly change. Units of plot are in fraction of areosynchronous Orbit Radius (compare Gassend, 2004)
- Tether angles off the vertical ~28° (20 GPa) and ~40.7° (10 GPa)
- Pavload goes with the Cos of tether angle!



 $= -\alpha \left(\vec{\tilde{g}} (\vec{\tilde{r}}) \right)$

Mars Lift, Curvature, Pinnacle Station



- Lower latitude of 12.65° vs. 18° => less curvature of the elevator => tether angles: ~20° (20 GP) and ~28.5° (10 Gpa)
- Still clears Phobos orbit comfortably by a factor of ~1.8 of the orbit change in this first calculation.
- If dust is tolerable, the lower latitude site offers integration advantages for the Omaha Trail.



Mars Lift, Counterweight



- The safest option appears to terminate Mars Lift inside the Deimos orbit, e.g., at ~23000 km radius, put the top Ares station at ~400-500 km inside Deimos orbit.
- Bracketing the counterweight mass preliminarily for this situation:

 - A 20 Gpa tether has at areostationary Orbit approximately that strength and that counterweight condition should not be exceeded.
- The Geometry Condition leads to a relatively strong elevator, variations of the counterweight mass scenario are still investigated.
- Putting the counterweight mass further out, e.g., past Deimos, will help to reduce the counterweight mass if necessary.
- Keep Ares Station close to Deimos for efficient transfers.





Mars Lift, Deployment and Anchor Forces



- Expected is a ground force of up to10⁶ N for a functional elevator and to pull it into place for deployment.
- A large tractor (e.g., group of tanks) will have to pull the elevator to position or it will have to be deployed in its lightest form (TBD) and to be built up.
- How can an off equator configuration be kept stable while the elevator is built up, including building the counterweight?
- It is an advantage that the counterweight mass can be iteratively increased by transporting material from Deimos.
- It is easier to build from above.



Mars Lift, Summary



- A simplified feasibility condition using rappellers and only going down, no motor or large power source required.
- The energy gained going down could possibly be used to build up (e.g., fuse new material to) or protect (e.g., clean/sweep) the Mars Lift elevator.
- To Do:
 - Look for further minimization of Elevator requirements
 - Investigate ideas for elevator protection and growth
 - Investigate deployment scenarios
- Thanks to the all supporters!





References

Disclaimer: All presented results are first approximations and may undergo corrections without notice.

- LakeMatthew.com
- Most astrodynamics data via Wolfram system (Mathematica, etc.)
- nasa.gov
- Background artwork: Kees Veenenbos, <u>www.space4case.com</u> and data: MOLA Science Team (NASA)
- MarsTrek site, JPL
- Google Earth, Mars Maps
- Tethers for Mars Space Operations. The Case for Mars II. 62 Science and Technology Series. pp. 445–465, Penzo, July 1984.
- Non-Equatorial Uniform-Stress Space Elevators, Gassend, 2004, including presentation on Off-equator space elevators and C code.
- Lunar Frontier Transportat System, Pearson et al., 2007
- Lunar Tether Transport, Levin, in Lunar Space Elevators for Cislunar Space Development, Pearson, 2005
- High Altitude Dust Global Distribution, Vertical Mixing, and Particle Sizes During the 2001 Planet-Encircling Dust Storm, Clancy, 2008
- The Schumann resonance: A tool for exploring the atmospheric environment and the subsurface of the planets and their satellites, Simoes et al, 2008
- Martian satellite orbits and ephemerides, Jacobson/Lainey, 2014



Mars Lift (ML)

Lake Matthew Team / Celestia

Mars Lift (ML)

Rappeller heat management:

- Brakes must counter gravitational acceleration
- Friction brakes would quickly overheat
- Eddy current brakes can work, but radiators are required



Mars Lift (ML)

- Rappeller design considerations:
 - Unpowered descent for cargo delivery
 - Should be a mass-produced vehicle, easily repaired at Omaha Crater
 - Lightweight, with compact storage
 - Notional 10-ton payload (5 tons x 2)



4.4 m

Omaha Trail to Lake Matthew

Rationale for the Omaha Trail MATT: The Mars Terraformer Transfer Omaha Crater: Cargo & Propellant Deimos ISRU, Deimos Dock Deimos Rail Launcher (DRL) Mars Lift-(ML)

Tramway

Omaha Trail Benefits MATT + Omaha Trail

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Tramway

• Conceptual design in the spirit of lunar tramway (Pearson et al. 2005)



Tramway

- ISRU alloy pylons
- CNT cables with Omaha Crater HVDC power
- Notionally 10x60 mm² cable cross-section with 70 kN tensioning
- 30+ km pylon separation, peak-spanning, 400+ m pylon height
- The rappeller should be designed to convert into HVDC tramway "trammer"



Omaha Trail to Lake Matthew

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ramway

Omaha Trail Benefits

MATT + Omaha Trail

Omaha Trail (With Tankers) Cuts Propellant ~86%





Omaha Trail Benefits

- Cuts Earth cargo/tanker launches by 83%
- Cuts propellant requirement ~86%
- 100% of Omaha Crater power would be freed for use on Mars



Crew Benefits

- Crewed Earth-return on the Omaha Trail:
 - Faster crew return: All propellant for Earth insertion, cutting transit time by more than half, thereby cutting cosmic radiation exposure by more than half
 - 300+ tons of water shielding: Deimos water adds 1 m+ depth of shielding to block all cosmic rays < 20 MeV, and at higher MeV block 2/3 of neutrons, 1/3 of muons and 1/3 of protons



Crew Benefits

• Crewed Earth-return on the Omaha Trail:



guayo et al. 201

Figure 27: Cosmic Proton Flux through Water

Crew Benefits

- Crewed Earth-return on the Omaha Trail:
 - Faster crewed ITS return: Omaha Trail reserves all propellant for Earth insertion burn, cutting transit time by more than half, and cutting cosmic radiation exposure by more than half
 - 300+ tons of water radiation shielding: Deimos ISRU water can give an extra 1 m depth of shielding to block all cosmic rays < 20 MeV, and at higher MeV block 2/3 of neutrons, 1/3 of protons, and 1/3 of muons
 - Fast return with extra water shielding cuts radiation exposure >80%, preventing career-limiting exposure



Omaha Trail to Lake Matthew

Rationale for the Omaha Trail:

- It would reduce Earth launches (83%)
- It would lower transport cost (opportunity for Omaha Trail Consortium)
- It orchestrates and justifies R&D for each infrastructure component (Deimos ISRU -> Deimos Dock -> DRL -> ML -> tramway)
- Fast crew return with less radiation exposure (cuts transit time in half, and cuts cosmic radiation exposure >80% to prevent career-limiting exposure)

Omaha Trail to Lake Matthew

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Omaha Trail Benefits MATT + Omaha Trail

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MATT Cuts Earth Cargo Launches ~ 90%

- Habs 2 orders of magnitude larger than reference, with same cargo mass
- ISRU self-sufficiency in many massive products
- Cuts cargo mass, and cuts Earth launches of cargo/tankers, ~90%


MATT + Omaha Trail

Rationale for combining:

- MATT terraforming cuts Earth cargo launches by ~90%, for affordable, robust facilities
- MATT and Omaha Trail together cut required Earth cargo launches by >95%, and enable:
 - Multiple martian settlements
 - Rapid planet-wide exploration
 - Extensive commercial development
 - Faster, safer crew transport home



Omaha Trail to Lake Matthew

Thank you!

Lake Matthew Team / Celestia

Links

Lake Matthew – <u>LakeMatthew.com</u>

New Space Journal – <u>liebertpub.com/overview/new-space/610</u>

References

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Aguayo, E., Kouzes, R. T., Ankney, A. S., Orrell, J. L., Berguson, T. J., & Troy, M. D. (2011). Cosmic ray interactions in shielding materials. Pacific Northwest National Laboratory Report No. PNNL-20693.

Davis, A. M. (Ed.). (2005). Meteorites, Comets, and Planets: Treatise on Geochemistry (Vol. 1). Elsevier.

D'Orazio, M., & Folco, L. (2003). Chemical Analysis of Iron Meteorites by Inductively Coupled Plasma-Mass Spectrometry. Geostandards and Geoanalytical Research, 27(3), 215-225.

Engel, T. G., Timpson, E. J., & Veracka, M. J. (2015). Demonstration of a reversible helical electromagnetic launcher and its use as an electronically programmable mechanical shock tester. *IEEE Transactions on Plasma Science*, 43(5), 1266-1270.

Engel, T. (2004). U.S. Patent No. 6,696,775. Washington, DC: U.S. Patent and Trademark Office.

Fanale, F. P., & Salvail, J. R. (1990). Evolution of the water regime of Phobos. Icarus, 88(2), 380-395.

Gay, S. E. (2010). Contactless magnetic brake for automotive applications (Doctoral dissertation, Texas A & M University).

Hoashi, M., Brooks, R. R., & Reeves, R. D. (1993). Palladium, platinum and ruthenium in iron meteorites and their taxonomic significance. Chemical geology, 106(3-4), 207-218.

Hughes, G. B., Lubin, P., Bible, J., Bublitz, J., Arriola, J., Motta, C., ... & Wu, J. (2013). DE-STAR: phased-array laser technology for planetary defense and other scientific purposes.

Lubin, P., Hughes, G. B., Eskenazi, M., Kosmo, K., Johansson, I. E., Griswold, J., ... & Riley, J. (2016). Directed energy missions for planetary defense. Advances in Space Research, 58(6), 1093-1116.

Murchie, S. L., Fraeman, A. A., Arvidson, R. E., Rivkin, A. S., & Morris, R. V. (2013). Internal characteristics of Phobos and Deimos from spectral properties and density: relationship to landforms and comparison with asteroids.

Nichols, C. R. (1993). Volatile products from carbonaceous asteroids. *Resources of near-earth space*, 543-568.

Pearson, J., Levin, E., Oldson, J., & Wykes, H. (2005). Lunar space elevators for cislunar space development. NASA Institute for Advanced Concepts Study Technical Report, 7.

Schwenzer SP, Abramov O, Allen CC, Clifford SM, Cockell CS, Filiberto J, Kring DA, Lasue J, McGovern PJ, Newsom HE, Treiman AH. "Puncturing Mars: How impact craters interact with the Martian cryosphere." Earth and Planetary Science Letters. 2012 Jun 15;335:9-17.

Shen, J. J., Papanastassiou, D. A., & Wasserburg, G. J. (1996). Precise Re-Os determinations and systematics of iron meteorites. Geochimica et Cosmochimica Acta, 60(15), 2887-2900.

Image Credits

Blair, Jonathan S. / National Geographic / Getty Images: Eden Project greenhouse, Cornwall, England Celestia Software: Simulated imagery of Mars system Celle, Ludovic: Mars illustration Clark, Chuck: natural boundary mapping of Deimos HiRISE / MRO / LPL (U. Arizona) / NASA: Deimos imagery NASA / JPL-Caltech / Malin Space Science Systems: Mars imagery Öner, Tayfun / USGS / Thomas, Peter: Deimos mappings and orthographic renderings Pearson et al. 2005: Lunar Space Elevator and Tramway Pioneer Astronautics: CAVoR visualization SpaceX: ITS visualizations SSL / ASU /P. Rubin / NASA / JPL-Caltech: 16 Psyche artist's concept Toshiba / Chubu Electric: SMES unit U.S. Navy: F-14 on catapult Wood, Roy: Surprise Lake inside Aniakchak Caldera Veenenbos, Kees: Olympos Mons rendering: www.space4case.com, and Data: MOLA Science Team (NASA)